

AD-A148 394

NEAR AXIS SHIP WAKES(U) MITRE CORP MCLEAN VA K M CASE  
AUG 84 JSR-84-203C F19628-84-C-0001

1/1

AUG 84 JSR-84-203C F19628-84-C-0001

UNCLASSIFIED

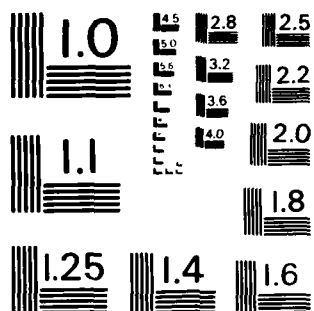
F/G 20/4

NL

END

40 MED

DTMC



MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS-1963-A

AD-A148 394

FILE COPY

84 12 10 093

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM	
1. REPORT NUMBER JSR-84-203C	2. GOVT ACCESSION NO. <b>A148 394</b>	3. RECIPIENT'S CATALOG NUMBER	
4. TITLE (and Subtitle)  Near Axis Ship Wakes		5. TYPE OF REPORT & PERIOD COVERED	
7. AUTHOR(s)  K. M. Case		6. PERFORMING ORG. REPORT NUMBER	
9. PERFORMING ORGANIZATION NAME AND ADDRESS The MITRE Corporation 1820 Dolley Madison Blvd. McLean, VA 22102		8. CONTRACT OR GRANT NUMBER(s)  F19628-84-C-0001	
11. CONTROLLING OFFICE NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS	
14. MONITORING AGENCY NAME & ADDRESS (if diff. from Controlling Office)		12. REPORT DATE August 1984	13. NO. OF PAGES 31
		15. SECURITY CLASS. (of this report)  Unclassified	
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE	
16. DISTRIBUTION STATEMENT (of this report)  <div style="border: 1px solid black; padding: 5px; text-align: center;"> <b>DISTRIBUTION STATEMENT A</b>            Approved for public release            Distribution Unlimited         </div>			
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from report)			
18. SUPPLEMENTARY NOTES			
19. KEY WORDS (Continue on reverse side if necessary and identify by block number)			
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) <p>This report studies the structure of a ship surface wave wake far down stream in the vicinity of the axis. Of particular interest is the effects of finite ship width.</p> <p>The theoretical work shows that there are singularities in the flow field but they are not on the axis. It is argued that the singularity is not real but is rather due to an injudicious rise of the stationary phase method.</p>			

DD FORM 1 JAN 73 **1473**

EDITION OF 1 NOV 65 IS OBSOLETE

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

---

# Near Axis Ship Wakes

---

K. M. Case

August 1984

JSR-84-203C

Approved for public release. distribution unlimited

DTIC  
ELECTE  
S DEC 10 1984 D  
B

JASON  
The MITRE Corporation  
1820 Dolley Madison Boulevard  
McLean, Virginia 22102

## NEAR AXIS SHIP WAKES

### I. Introduction

The problem we address is that of the structure of a ship surface wave wake far down stream in the vicinity of the axis, (i.e.:  $\frac{L}{X}, \frac{Y}{X} \ll 1$ , where  $L$  is a typical dimension of the ship).

Basic approximations made are:

- (i) The linearized theory is used.
- (ii) It is assumed that  $g L/U^2 \gg 1$ . Further, rather conventional stationary phase methods are employed. It is indicated that this is the most suspect part of the calculation. Elucidation is warranted.

We are particularly interested in the effects of finite ship width. Accordingly, we deal with a simplified hull model. It is one of a prolate semi-spheroid. This has the advantage that the underlying potential flow is simple and can be written in closed form.

The main conclusions obtained are:

- 1) In agreement with other calculations it is found that singularities appear in the flow field. However, the singularity is not on the axis but is displaced therefrom. (In our model the displacement is of the order of the ship width.)
- 2) It is argued that the singularity is not real, but is rather due to an injudicious rise of the stationary phase method. However, it is probable that the singularity indicates that large disturbances can result far from the Kelvin angle and yet not on the axis.



Accession For	
NTIS GRA&I	<input checked="" type="checkbox"/>
DTIC TAB	<input type="checkbox"/>
Unannounced	<input type="checkbox"/>
Justification	
By	
Distribution/	
Availability Codes	
Dist	Avail and/or Special
A-1	

## II. The Basic Equations

### 1. The Integral Representation

These are as in reference (1). We use the linearized Euler equations and boundary conditions. In a coordinate system at rest with respect to the ship we can write the velocity potential as

$$\phi = Ux + \phi \quad (1)$$

(U is the velocity of the ship which is moving in the + x direction).

Then  $\phi$  satisfies

$$\nabla^2 \phi = 0, \quad (2)$$

$$\frac{\partial \phi}{\partial n} = -n_x U \text{ (on the ship surface)} \quad (3)$$

and 
$$\frac{\partial^2 \phi}{\partial x^2} + \frac{g}{U^2} \frac{\partial \phi}{\partial z} = 0 \text{ (on the free ocean surface } z = 0) \quad (4)$$

If we introduce a Green's function satisfying



$$\nabla^{-2} G(\underline{r}', \underline{r}) = \delta(\underline{r}' - \underline{r}) \quad (5)$$

$$\text{and} \quad \frac{\partial G}{\partial z'}(\underline{r}', \underline{r}) + \frac{U^2}{g} \frac{\partial^2}{\partial X'^2} G(\underline{r}', \underline{r}) \Big|_{z'=0} = 0 \quad (6)$$

then using Green's identity we have the representation:

$$\begin{aligned} \phi(r) = & \int_{S_1} G(\underline{r}', r) \frac{\partial}{\partial n'} G(\underline{r}', r) dS_1 \\ & + \frac{U^2}{g} \int_{c^-} \phi(\underline{r}') \frac{\partial}{\partial X'} G(\underline{r}', r) - \frac{\partial \phi}{\partial X'} G(\underline{r}', \underline{r}) \Big|_{\substack{z'=0 \\ X'=X-(y')}} dy' \quad (7) \\ & - \frac{U^2}{g} \int_{c^+} \phi(\underline{r}') \frac{\partial}{\partial X'} G(\underline{r}', r) - \frac{\partial \phi}{\partial X'} G(\underline{r}', \underline{r}) \Big|_{\substack{z'=0 \\ X'=X+(y')}} dy' \end{aligned}$$

(Here  $S_1$  is the hull of the ship and  $c^+ + c^-$  is the waterline.)

The equation (7) plays two roles.

a) When  $\underline{r}$  is on  $S_1$  this is an inhomogeneous integral for  $\phi(\underline{r})$ .

b) When  $\underline{r}$  is not on  $S_1$  this gives an integral representation for  $\phi(\underline{r})$  in terms of its value and normal derivative on  $S_1$ .

Our basic approximation is then the following:

The  $G$  defined by equation (5) and (6) can be written as

$$G(\underline{r}', \underline{r}) = G_0(\underline{r}', \underline{r}) + G_1(\underline{r}', \underline{r}) \quad (8)$$

where

$$G_0(\underline{r}', \underline{r}) = \frac{1}{4\pi} \left\{ \frac{1}{|\underline{r}' - \underline{r}|} + \frac{1}{|\underline{r}' - \hat{\underline{r}}|} \right\} \quad (9)$$

with  $\hat{\underline{r}} = (x, y, -z)$ ,

and

$$G_1(\underline{r}', \underline{r}) = \frac{-1}{(2\pi)^2} \iint \frac{d^2k}{k[\frac{gk}{U^2} - k_x^2]} \frac{k_x^2}{e^{k(z+z')}} e^{i[k_x(x'-x) + k_y(y'-y)]} \quad (10)$$

where  $k = \sqrt{k_x^2 + k_y^2}$ .

When  $gL/U^2 \gg 1$  and  $\underline{r}, \underline{r}'$  are on  $S_1$ , we expect  $G_1 \ll G_0$ . Thus the integral equation (7) for  $\phi(\underline{r})$  with  $\underline{r}$  on  $S_1$  can be approximated by putting  $G = G_0$ . The integral equation which results is then that of a simple potential flow problem--which is readily solved yielding a solution  $\phi_0$ .

To calculate the radiated field (for  $r$  far from  $S_1$ ) we then replace  $\phi$  in equation (7) by  $\phi_0$  and  $G$  by  $G_1$ .

More precisely, we use the radiative part of  $G_1$ . This is obtained so: Causality tells us that the poles in equation (10) are to be above the contour of integration. The radiative part is just the contribution of the poles. For the part of  $G_1$  which generates the radiation field we then obtain

$$G_1 \sim -\frac{i}{2\pi} \frac{g}{U^2} \int_{-\infty}^{\infty} \frac{d\ell_y}{1-2\ell} \frac{\ell_x}{\ell} e^{\frac{g}{U^2} \ell(z+z')} e^{\frac{ig}{U^2} [\ell_x(x'-x) + \ell_y(y'-y)]} \quad (11)$$

+ complex conjugate

(Here we have introduced dimensionless variables

$$\text{so that } (k_x, k_y, k) = \frac{g}{U^2} (\ell_x, \ell_y, \ell) . . ) \quad (12)$$

## 2. Boat Model

We model the hull as half of a prolate spheroid. To be specific, introduce spheroidal coordinates so that

$$x = c \cosh \eta \cos \theta$$

$$y = c \sinh \eta \sin \theta \cos \omega$$

$$z = c \sinh \eta \sin \theta \sin \omega$$

Then the hull is the surface

$$\eta = \eta_0, \quad 0 \leq \theta \leq \pi, \quad \pi \leq \omega \leq 2\pi$$

(The major and minor axis are thus  $a = c \cosh \eta_0$ ,  $b = c \sinh \eta_0$ .)

The scale factors are

$$h_1 = h_2 = c \sqrt{\sinh^2 \eta \cos^2 \theta + \cosh^2 \eta \sin^2 \theta}$$

$$h_3 = c \sinh \eta \sin \theta,$$

or if we introduce  $\zeta = \cosh \eta$ ,  $\mu = \cos \theta$

$$h_1 = h_2 = c \sqrt{\zeta^2 - \mu^2}$$

$$h_3 = c \sqrt{(\zeta^2 - 1)(1 - \mu^2)}.$$

In reference (1) it is shown that

$$\phi_o = -\mu U c f(\zeta) \quad (13)$$

where

$$f(\zeta) = \frac{2 + \zeta \ln \left( \frac{\zeta-1}{\zeta+1} \right)}{\frac{2\zeta_o}{\zeta_o^2-1} + \ln \frac{(\zeta_o-1)}{(\zeta_o+1)}} \quad (14)$$

### III. Fundamental Integrals

In our approximation, we then have

$$\phi_{\text{asym}} = \sum_{i=1}^6 I_i \quad (15)$$

$$\text{where } I_1 = \frac{U^2}{g} \int_{c+} \frac{\partial \phi_0}{\partial x'} G(\underline{r}', \underline{r}) \Big|_{\substack{z'=0 \\ x'=x+(y')}} dy' \quad (16)$$

$$I_2 = - \frac{U^2}{g} \int_{c-} \frac{\partial \phi_0}{\partial x'} G_1 dy' \quad (17)$$

$$I_3 = \int_{S_1} \frac{\partial \phi_0}{\partial n'} G_1(\underline{r}', \underline{r}) dS_1 \quad (18)$$

$$I_4 = \frac{-U^2}{g} \int_{c+} \phi_0(\underline{r}') \frac{\partial}{\partial x'} G_1(\underline{r}', \underline{r}) dy' \quad (19)$$

$$I_5 = \frac{U^2}{g} \int_{c-} \phi_0(\underline{r}') \frac{\partial}{\partial x'} G_1(\underline{r}', \underline{r}) dy' \quad (20)$$

$$I_6 = - \int_{S_1} \phi_0 \frac{\partial}{\partial n'} G_1(\underline{r}', \underline{r}) dS_1 \quad (21)$$

Some useful kinematics:

$$\frac{\partial \phi_0}{\partial x'} = \frac{\mu(\zeta^2 - 1) \frac{\partial \phi_0}{\partial \zeta} + \zeta(1 - \mu^2) \frac{\partial \phi_0}{\partial \mu}}{c(\zeta^2 - \mu^2)} \quad (22)$$

$$\frac{\partial \phi_o}{\partial n'} = -\frac{1}{c} \sqrt{\frac{(\zeta_o^2 - 1)}{(\zeta_o^2 - \mu^2)}} \frac{\partial \phi_o}{\partial \zeta} \quad (23)$$

$$dS_1 = c^2 \sqrt{\zeta_o^2 - \mu^2} \sqrt{\zeta_o^2 - 1} \sin \theta \, d\theta \, d\omega. \quad (24)$$

Let us see how some typical integrals are to be evaluated.

Consider  $I_1$ . This is an integral over  $c+$ .  $c+$  is  $X' > 0$ ,  $Z' = 0$

$$\therefore 0 \leq \theta \leq \frac{\pi}{2}$$

For  $y' > 0$ , we have  $y' = b \sin \theta$ .

$$dy' = b \cos \theta \, d\theta$$

As  $y$  goes from 0 to  $b$ ,  $\theta$  goes from 0 to  $\frac{\pi}{2}$ .

For  $y' < 0$ , we have  $y' = -b \sin \theta$ ,  $dy' = -b \cos \theta \, d\theta$

As  $y'$  goes from  $-b$  to 0,  $\theta$  goes from  $\frac{\pi}{2}$  to 0.

$$\therefore I_1 = \int_0^\pi \cos \theta \, d\theta \frac{\partial \phi_0}{\partial x} \left\{ \begin{array}{l} G_1 (a \cos \theta, b \sin \theta, 0; \underline{r}) \\ + G (a \cos \theta, -b \sin \theta, 0; \underline{r}) \end{array} \right\} \quad (25)$$

Consider  $I_3$ .

Using equations (23) and (24) we have

$$\frac{\partial \phi_0}{\partial n} \, dS_1 = -c (\zeta_0^2 - 1) \frac{\partial \phi_0}{\partial \zeta} \sin \theta \, d\theta \, d\omega$$

and thus

$$I_3 = -c (\zeta_0^2 - 1) \int_0^\pi d\theta \sin \theta \frac{\partial \phi_0}{\partial \zeta} \int_\pi^{2\pi} d\omega G_1 (\underline{r}', \underline{r}) . \quad (26)$$

Now,

$$\int_\pi^{2\pi} d\omega G_1 = \frac{-1}{2\pi} \frac{g}{U^2} \int_{-\infty}^{\infty} \frac{d\ell_y \ell_x}{1-2\ell} e^{-\frac{1g}{U^2} [\ell_x x + \ell_y y]} e^{\frac{1g}{U^2} \ell_x a \cos \theta} \quad (27)$$

x J ,

$$\text{with } J = \int_\pi^{2\pi} d\omega e^{\frac{g\ell b}{U^2} \sin \theta \sin \omega} e^{\frac{g}{U^2} \ell_y b \sin \theta \cos \omega} \quad (28)$$



Clearly in our approximation of  $\frac{gb}{U^2} \gg 1$ , the principal contributions come from the vicinity of  $\omega = \pi, 2\pi$ .

Thus,

$$J \approx e^{\frac{-ig}{U^2} \ell_y b \sin \theta} \int_{\pi}^{\frac{3\pi}{2}} d\omega e^{\frac{g}{U^2} \ell b \sin \theta \sin \omega} \\ + e^{\frac{ig}{U^2} \ell_y b \sin \theta} \int_{\frac{3\pi}{2}}^{2\pi} d\omega e^{\frac{g}{U^2} \ell b \sin \theta \sin \omega}$$

In the first of these integrals, we let

$$\omega = \pi + \epsilon, \text{ then } d\omega = d\epsilon$$

$$\sin \omega = \sin(\pi + \epsilon) = -\cos \epsilon \approx -\epsilon.$$

$$\text{Then } \int_{\pi}^{\frac{3\pi}{2}} = \int_0^{\infty} d\epsilon e^{c \frac{-g \ell b \sin \theta \epsilon}{U^2}} = \frac{U^2}{g \ell b \sin \theta}.$$

Similarly,

$$\int_{\frac{3\pi}{2}}^{2\pi} = \frac{U^2}{g \ell b \sin \theta}$$

and thus

$$J = \frac{U^2}{g l b \sin \theta} \left\{ e^{i \frac{g}{U^2} l b \sin \theta} + e^{-i \frac{g}{U^2} l b \sin \theta} \right\}.$$

Inserting into equations (27) and (26) yields:

$$\begin{aligned} I_3 = U b \frac{\partial f}{\partial \zeta} \left( \frac{-1}{2\pi} \right) \int_{-\infty}^{\infty} \frac{d l_y l_x}{l (1-2l)} e^{-i \frac{g}{U^2} (l_x x + l_y y)} \\ \times \int_0^{\pi} \cos \theta d\theta \left\{ e^{i \frac{g}{U^2} [l_x a \cos \theta + l_y b \sin \theta]} \right. \\ \left. + e^{i \frac{g}{U^2} (l_x a \cos \theta - l_y b \sin \theta)} \right\} \end{aligned} \quad (29)$$

The remaining  $I_1$  are evaluated similarly. The results are:

$$\begin{aligned} I_1 + I_2 + I_3 = \frac{i U b}{2\pi} \int_{-\infty}^{\infty} \frac{d l_y l_x}{1-2l} e^{-i \frac{g}{U^2} (l_x x + l_y y)} \\ \times \int_0^{\pi} \cos \theta d\theta \left\{ \frac{\partial f}{\partial \zeta} \left[ \frac{\mu^2 (\zeta_0 - 1)}{\zeta_0^2 - \mu^2} - \frac{1}{l} \right] + \frac{\zeta_0 f [1 - \mu^2]}{(\zeta_0^2 - \mu^2)} \right\} \{ e^+ + e^- \}. \end{aligned} \quad (30)$$

+ c. c.

and

$$I_4 + I_5 + I_6 = \frac{U}{2\pi} \frac{b g}{U^2} \text{cf} \int_{-\infty}^{\infty} \frac{d l_y l_x}{1-2l} e^{-i \frac{g}{U^2} (l_x x + l_y y)}$$

$$\begin{aligned}
& \times \int_0^\pi \cos \theta \, d\theta \left\{ l_x \cos \theta \left(1 - \frac{1}{\ell}\right) [e^+ + e^-] \right. \\
& - \frac{ig}{b} \left(\frac{U^2}{gb}\right) \frac{1}{\ell} [e^+ + e^-] \\
& \left. - \frac{l_y}{\ell} \frac{g}{b} \sin \theta [e^+ - e^-] \right\}
\end{aligned} \tag{31}$$

+ c.c.

$$\left( \text{Here } e^\pm = e^{i \frac{g}{U^2} [l_x a \cos \theta \pm l_y b \sin \theta]} \right)$$

#### IV. The Stationary Phase Evaluation

So far the approximations made are:

(i) Linearization

(ii)  $\phi \rightarrow \phi_0$  on  $S_1$ . This justified by the assumption  $gL/U^2 \gg 1$ .

(iii) In the integrals over  $S_1$  only the immediate vicinity of the surface contributes significantly. Again this is justified by  $gL/U^2 \gg 1$ .

We are left with generic integrals of the form

$$I_{\pm} = \int_{-\infty}^{\infty} dl_y g(l_y) e^{-i \frac{g}{U^2} (l_x x + l_y y)} \times \int_0^{\pi} h(\theta) e^{i \frac{g}{U^2} [l_x a \cos \theta \pm l_y b \sin \theta]} d\theta \quad (32)$$

(Remember:  $l_x = \sqrt{l}$ ,  $l = \sqrt{l_x^2 + l_y^2}$ .)

We want to evaluate these integrals in the limits  $|y/x| \ll 1$ ,  $|b/x| \ll 1$ . Our approach is to use the method of stationary phase twice.

First we do the  $\theta$  integral by stationary phase. The stationary points  $\theta_{\pm}^+$  are then functions of  $l_y$ . The  $l_y$  integral is then done by another application of stationary phase.

The main result is that in the limit of interest there are two classes of stationary points.

$$(a) \quad l \sim l_x \sim 1, \quad l_y \sim 0, \quad \cos^2 \theta_0 \approx 1$$

$$(b) \quad l \sim l_y \gg l_x \gg 1, \quad \cos^2 \theta_0 \approx 0$$

In the integrals  $I_{\pm}^+$ , we first encounter

$$\int_0^{\pi} h(\theta) e^{i \phi_{\pm}^+}$$

$$\text{where } \phi_{\pm}^+ = \frac{g}{U^2} [l_x a \cos \theta \pm l_y b \sin \theta]$$

The stationary phase condition  $\frac{\partial \phi_{\pm}^+}{\partial \theta} = 0$

$$\text{yields } \tan \theta_{\pm}^+ = \pm \frac{l_y}{l_x} \frac{b}{a} \quad (33)$$

Then

$$\int_0^\pi h(\theta) e^{i\phi_\pm} = e^{i\phi_\pm(\theta_+)} h(\theta_+) \int_{-\infty}^{\infty} e^{\frac{-1}{2}(\theta-\theta_+)^2} \phi_\pm(\theta_+) d\theta.$$

Then

$$I_\pm = \int_{-\infty}^{\infty} g(l_y) h(\theta_\pm) \left[ \int_{-\infty}^{\infty} e^{\frac{-1}{2}(\theta-\theta_\pm)^2} \phi_\pm(\theta_\pm) d\theta \right] e^{-i\phi_\pm} \quad (34)$$

where

$$\phi_\pm = \frac{g}{u^2} [l_x(x - a \cos \theta_\pm) \mp l_y(y \mp b \sin \theta_\pm)] \quad (35)$$

The stationary phase condition  $\frac{\partial \phi}{\partial l_y} = 0$

yields

$$\frac{\partial l_x}{\partial l_y} = \frac{\pm b \sin \theta_\pm - y}{x - a \cos \theta_\pm} + \left[ \frac{\pm l_y b \cos \theta_\pm - l_x a \sin \theta_\pm}{x - a \cos \theta_\pm} \right] \frac{\partial \theta_\pm}{\partial l_y}. \quad (36)$$

We are interested only in cases where  $|x| \gg a$ . Therefore, we are always justified in taking as our basic equation

$$\frac{\partial l_x}{\partial l_y} = \frac{\pm b \sin \theta_\pm - y}{x} + \left[ \frac{\pm l_y b \cos \theta_\pm - l_x a \sin \theta_\pm}{x} \right] \frac{\partial \theta_\pm}{\partial l_y} \quad (37)$$

Since  $\theta_\pm$  are implicit functions of  $l_y$  via equation (33) this is in principle a very difficult equation to solve for  $l_y$ .

However, in our limit it is readily solved by a perturbation theory. We assume the second term on the right is small compared to the first. Calculate  $\ell_y$  using only the first term and then verify that the second term is indeed small.

Thus, in first approximation our equation is

$$\frac{\partial \ell_x}{\partial \ell_y} = \theta_{\pm} \quad , \quad (38)$$

where  $\theta_{\pm} = \frac{\pm b \sin \theta_0 - y}{x}$ , and by assumption

$$|\theta_{\pm}| \ll 1.$$

Since 
$$\frac{\partial \ell_x}{\partial \ell_y} = \frac{\ell_y}{\ell_x (2\ell - 1)}$$

Our basic equation (38) becomes

$$\frac{\ell_y}{\ell_x (2\ell - 1)} = \theta_{\pm} \quad (39)$$

Squaring gives

$$\frac{\ell_y^2}{\ell_x^2 (2\ell - 1)^2} = \theta_{\pm}^2 \quad . \quad (40)$$

If we note that  $\ell_y^2 = \ell(\ell-1)$ ,  $\ell_x^2 = \ell$  and set  $2\ell - 1 = A$ , we obtain a quadratic equation for A which can be solved to give

$$A = \frac{1 \pm \sqrt{1 - 8\theta_{\pm}^2}}{4\theta_{\pm}^2} . \quad (41)$$

Clearly, the two solutions correspond to the wave trains whose caustics give the classical Kelvin  $19\frac{1}{2}^\circ$  cone.

First, we look at the  $-$  in equation (41). This gives us the simplest (and least interesting) of the two wave sets. For small  $\theta$  this gives

$$A \approx 1 - 2\theta^2 .$$

$$\text{Then } \ell = \frac{A+1}{2} \approx 1 - \theta^2 \quad (42)$$

$$\text{and } \ell_x = \sqrt{\ell} \approx 1 - \frac{\theta^2}{2} , \quad (43)$$

From equation (39) we then see that

$$\ell_y \approx \theta_{-} \quad (44)$$



What does this imply for  $\theta_0$  ? The equation (33) tells us that

$$\tan \theta_{\pm} \approx \pm \theta \frac{b}{a} \quad (45)$$

Thus  $\theta_{\pm}$  is close to either 0 or  $\pi$  depending on the sign of the right side of equation (45).

Then  $\theta_{\pm} \approx -y/x$  . (Here  $x < 0$  and we will always look at  $y > 0$  .)

Then  $\theta_{+} = \theta = -y/x$

$$\theta_{-} = \pi - \epsilon$$

and solving for  $\epsilon$  we obtain

$$\epsilon = \theta = -y/x , \text{ i.e. } \theta_{-} = \pi - \theta$$

Then  $\phi_{\pm}(\theta_{\pm}) = \pm \frac{ga}{U^2}$  .

From this it follows that

$$\int_{-\infty}^{\infty} e^{-\frac{1}{2}(\theta - \theta_{\pm})^2} \phi_{\pm}(\theta_{\pm}) d\theta = \sqrt{\frac{2\pi U^2}{ga}} e^{\pm i\pi/4}$$

$$I_{\pm} = \sqrt{\frac{2\pi U^2}{ga}} e^{\pm i \frac{\pi}{4}} h(\theta_{\pm}) g(\theta) e^{-i \phi_{\pm}(\theta, \theta_{\pm})} \\ \times \int_{-\infty}^{\infty} e^{-i(\ell_y - \ell_y^0)^2 \frac{1}{2}} \frac{\partial^2 \phi}{\partial \ell_y^2} d\ell_y.$$

In our approximation

$$\frac{\partial^2 \phi}{\partial \ell_y^2} \approx \frac{g}{U^2} \times \frac{\partial^2 \ell_y}{\partial \ell_y^2} = \frac{gx}{U^2}.$$

$$\text{Thus, } I_{\pm} = \sqrt{\frac{2\pi U^2}{ga}} \sqrt{\frac{2\pi U^2}{g(-x)}} e^{i \frac{\pi}{4}} e^{\pm i \frac{\pi}{4}} g(\theta) h(\theta_{\pm}) e^{-i \phi_{\pm}}. \quad (46)$$

$$\text{Here } \phi_{\pm}(\theta, \theta_{\pm}) = \frac{g}{U^2} \left[ x \mp a - \frac{y^2}{x} \right]$$

Now let us turn to the solution of equation (41) taking the + sign. Thus,

$$A = \frac{1 + \sqrt{1 - 8 \theta_{\pm}^2}}{4 \theta_{\pm}^2} \approx \frac{1}{2 \theta_{\pm}^2}$$

$$\text{Then } \ell = \frac{A+1}{2} \approx \frac{1}{4 \theta_{\pm}^2}$$

$$\ell_x = \frac{1}{2 |\theta_{\pm}|}$$

$$\ell_y = \theta_{\pm} \ell_x (2\ell - 1) = \frac{\text{sgn } \theta}{4 \theta^2}$$

The equation for the  $\theta_{\pm}$  are

$$\tan \theta_{\pm} = \pm \frac{b}{a} \frac{1}{2\theta_{\pm}} .$$

To be definite, let us discuss the case

$$y > b. \text{ Then } \theta_{\pm} > 0 .$$

$\theta_{+}$  ( $\theta_{-}$ ) is then just less than (greater than)  $\pi/2$  .

Explicitly,

$$\theta_{+} = \frac{\pi}{2} - \frac{2\theta_{+} a}{b}$$

$$\theta_{-} = \frac{\pi}{2} + \frac{2\theta_{-} a}{b}$$

Substituting in the expressions for  $\phi_{\pm}(\theta_{\pm})$  yields

$$\phi_{\pm}(\theta_{\pm}) = \pm \frac{g}{U^2} \frac{b}{4\theta_{\pm}^2}$$

and then

$$\int_{-\infty}^{\infty} \frac{1}{2} (\theta - \theta_{\pm})^2 \phi_{\pm}(\theta_{\pm}) d\theta$$

$$= \sqrt{\frac{\infty \pi U^2 \theta_{\pm}^2}{gb}} e^{+i\pi/4}$$

$$I_{\pm} = \sqrt{\frac{\infty \pi U^2 \theta_{\pm}^2}{gb}} e^{+i\pi/4} e^{-i\phi_{\pm}(\theta_{\pm}, \theta_{\pm})}$$

$$\int_{-\infty}^{\infty} e^{\frac{i}{2} (\ell_y - \ell_y)^2} \frac{\partial^2 \phi}{\partial \ell_y^2} d\ell_y$$

Here  $\phi_{\pm} = \frac{g}{U^2} [\ell_x x - \ell_y (\pm b \sin \theta_{\pm} - y)]$

Using the expressions for  $\ell_x$ ,  $\ell_y$ ,  $\theta_{\pm}$  in terms of  $\theta_{\pm}$  simplifies this to

$$\phi_{\pm} = \frac{g}{4U^2} \frac{x}{\theta_{\pm}}$$

To lowest order (in  $\theta$ ) we have

$$\frac{\partial^2 \phi}{\partial \ell_y^2} \approx \frac{gx}{U^2} \frac{\partial^2 \ell_x}{\partial \ell_y^2}$$

But  $\frac{\partial^2 \ell_x}{\partial \ell_y^2} \approx -2 \theta_{\pm}^3$

$$\therefore \int_{-\infty}^{\infty} e^{\frac{-i}{2} (\ell_y - \ell_y^0)^2} \frac{\partial^2 \phi}{\partial \ell_y^2} d\ell_y = \sqrt{\frac{\pi U^2}{g(-x) \theta_{\pm}^3}} e^{-i\pi/4}$$

The results for  $I_{\pm}$  are then

$$I_{\pm} = \frac{2\pi U^2}{g} e^{\pm i\frac{\pi}{4}} e^{-i\frac{\pi}{4}} \sqrt{\frac{2}{b(-x) \theta_{\pm}}} \quad (47)$$

$$x e^{\frac{-igx}{4U^2 \theta_{\pm}}} g(\theta_{\pm}) h(\theta_{\pm})$$

To recapitulate:

$$\theta_{\pm} = \frac{\pm b - y}{x}$$

$$\theta_{+} = \frac{\pi}{2} - \frac{2 \theta_{+} a}{b}$$

$$\theta_{-} = \frac{\pi}{2} + \frac{2 \theta_{-} a}{b}$$

$$\ell = \frac{1}{4\theta_{\pm}} \approx \ell_y, \quad \ell_x = \frac{1}{2\theta_{\pm}}$$

(Remember we have assumed  $y \geq b$  !)

V. Explicit Forms

A. The Contributions From The Stationary Point Where

$$\ell \sim \ell_x \sim 1, \ell_y \sim \theta$$

Here  $\theta = -y/x$ .

and  $\theta_+ = \theta, \theta_- = \pi - \theta$ .

From the results of Section IV, it is readily seen that all of  $I_1 + I_2 + I_3$  vanish at least as  $\theta^2$ .

The only term in  $I_4 + I_5 + I_6$  which does not vanish similarly is

$$I = \frac{U}{2\pi} c f i \frac{a}{b} \int_{-\infty}^{\infty} \frac{d\ell_y \ell_x}{\ell(1-2\ell)} e^{-i \frac{g}{U^2} (\ell_x x + \ell_y y)} \\ \times \int_0^{\pi} \cos \theta d\theta [e^+ + e^-], \quad + c.c.$$

Using equation (46) we then find

$$I = -U c f i \frac{U^2}{gb} \sqrt{\frac{a}{(-x)}} e^{+i\frac{\pi}{4}} \quad (48)$$

$$\left\{ e^{-i\frac{\pi}{4}} e^{-\frac{ig}{U^2} \left(x - a - \frac{y^2}{x}\right)} - e^{+i\frac{\pi}{4}} e^{-\frac{ig}{U^2} \left[(x+a) - \frac{y^2}{x}\right]} \right\}$$

#### B. Contributions From the Far Stationary Point

Here  $\ell \approx \frac{1}{4\theta_{\pm}^2}$ ,  $\ell_y \approx \frac{1}{4\theta_{\pm}^2}$ ,  $\ell_x \approx \frac{1}{2\theta_{\pm}}$

$$\theta_{+} = \frac{\pi}{2} - 2 \frac{\theta_{+} + a}{b}, \quad \theta_{-} = \frac{\pi}{2} + 2 \frac{\theta_{+} a}{b}$$

$$\theta_{+} = \frac{+b - y}{x}.$$

Then

$$\sin \theta_{+} = 1 + O(\theta_{+}^2)$$

$$\cos \theta_{+} = \pm 2 \frac{\theta_{+} + a}{b} + O(\theta_{+}^3)$$

One might suspect that because of the overall factor of  $(\theta_{+})^{-1/2}$  in equation (47) that there may be singularities in some derivatives of our potential. However, it can be shown that almost all the terms in equations (30) and (31) are at worst of order  $\theta^{7/2}$

We consider two examples:

(a). The term in equation (30) proportional to

$$\int_0^\pi \cos \theta \, d\theta \frac{\partial f}{\partial \zeta} \left[ \frac{\mu^2 (\zeta_0^2 - 1)}{\zeta_0^2 - \mu^2} - \frac{1}{\ell} \right] \quad (49)$$

By our rules  $\mu^2$  and  $\frac{1}{\ell}$  are of order  $\theta^2$ . The multiplicative  $\cos \theta$  makes the expression  $\sim \theta^3$ . The factor  $\frac{\ell_x}{1-2\ell}$  gives another  $\theta$ . Finally the overall  $\theta^{1/2}$  shows that the contribution to  $\phi$  is  $\sim \theta^{7/2}$ .

(b) Somewhat more subtle is the evaluation of the terms in equation (31) proportional to

$$\int_0^\pi \cos \theta \, d\theta \left\{ \ell_x \cos \theta [e^+ + e^-] - \frac{\ell_y}{\ell} \frac{a}{b} \sin \theta [e^+ - e^-] \right\} \quad (50)$$

The terms  $\sim [e^+ + e^-]$  and  $[e^+ - e^-]$  separately are of order  $\theta$ .

However, there is a cancellation such that the overall expression is  $\sim \theta^3$ . Thus consider

$$\begin{aligned} & \int_0^\pi \cos \theta \, d\theta \left\{ \ell_x \cos \theta - \frac{\ell_y}{\ell} \frac{a}{b} \sin \theta \right\} e^+ \\ & \sim \cos \theta_+ \left\{ \frac{\cos \theta_+}{2\theta_+} - \frac{a}{b} \sin \theta_+ \right\} e^+ \end{aligned}$$



$$= \frac{2\theta_+ a}{b} \left\{ \frac{2\theta_+}{2\theta_+} \frac{a}{b} - \frac{a}{b} \right\} e^+ = 0 \text{ to } 0 (\theta^3) !$$

As a consequence we see that the dominant contribution for  $\theta \ll 1$  is:

$$\begin{aligned} \phi &= \frac{iUb}{2\pi} \int_{-\infty}^{\infty} \frac{d\ell_y \ell_x}{1-2\ell} e^{\frac{-ig}{U^2} [\ell_x x + \ell_y y]} \\ &\times \int_0^{\pi} \cos \theta d\theta \zeta_0 f(\zeta_0) \frac{[1-u^2]}{(\zeta_0^2 - u^2)} [e^+ + e^-] \quad (51) \\ &+ \text{c.c.} \end{aligned}$$

Using our rules for integration this becomes

$$\begin{aligned} \phi &= -2Ua \frac{U^2}{g} \sqrt{\frac{2}{b(-x)}} \frac{f(\zeta_0)}{\zeta_0} \\ &\times \left\{ \theta_+^{\frac{3}{2}} e^{\frac{-igx}{4U^2 \theta_+}} + i \theta_-^{\frac{3}{2}} e^{\frac{-igx}{4U^2 \theta_-}} \right\} \quad (52) \\ &+ \text{c.c.} \end{aligned}$$

## VI. Discussion

We conclude that with our approximations the dominant term for the potential near the axis is given by equation (52). This has a singularity at  $y = b$  not at  $y = 0$ .

The potential and displacement at the singularity are both zero. But the slopes are infinite.

Where does the singularity come from? We think not from our use of the approximation  $U^2/gL \ll 1$ . Indeed tracing back to the origin of the term we see it arises from  $\partial\phi/\partial x$  on the waterline. Our procedure guarantees that  $\partial\phi/\partial x$  there is represented exactly.

Rather the origin would seem to result from an inappropriate use of the stationary phase method when evaluating equation (51). (This does not seem to matter for all other terms of equations (30) and (31). They are multiplied by a high powers of the vanishing quantity.) The problem with evaluating equation (51) by stationary phase is that  $\frac{\partial^2 \phi}{\partial k_y^2} \rightarrow 0$  as  $\Theta_+ \rightarrow 0$ .

Normally one would handle such a situation by proceeding to the next term in the Taylor series of  $\phi$  around the stationary

point. Thus instead of the Fresnel type integral one would have an Airy integral to describe the result in the vicinity of the bogus singular point. Here, however, one readily shows that not only does  $\frac{\partial^2 \phi}{\partial \ell^2} \rightarrow 0$  but so does  $\frac{\partial^3 \phi}{\partial \ell^3}$ . Indeed all higher derivatives go to zero as  $y_{\theta_+} \rightarrow 0$ . (They even go to zero faster and faster as the derivative increases.)

We conclude:

(1) The result of equation (52) would seem to indicate that there are large slopes in the wake near but not on the axis.

(2) A definitive conclusion (of the linear theory) awaits a better evaluation of the integrals of equation (51).

(3) Since we have used a very specific hull model it is not immediately obvious as to what the shape dependence really is. However, the procedure outlined here strongly suggests that large slopes should be produced in the wake at distances from the axis comparable to some measure of the ship width.

# REFERENCES

1. JSR-83-203, Section 4.

DISTRIBUTION LIST

Dr. Marv Atkins  
Deputy Director, Science & Tech.  
Defense Nuclear Agency  
Washington, D.C. 20305

National Security Agency  
Attn RS: Dr. N. Addison Ball  
Ft. George G. Meade, MD 20755

Mr. Anthony Battista [3]  
House Armed Services Committee  
2120 Rayburn Building  
Washington, D.C. 20515

Mr. Steve Borchardt  
Dynamics Technology  
Suite 200  
22939 Hawthorne Boulevard  
Torrance, CA 90505

Mr. Rod Buntzen  
NOSC  
Code 1603B  
San Diego, CA 92152

Dr. Curtis G. Callan, Jr.  
Department of Physics  
Princeton University  
Princeton, NJ 08540

Mr. Gerald Cann  
Principal Assistant Secretary  
of the Navy (RES&S)  
The Pentagon, Room 4E736  
Washington, D.C. 20350

Dr. Kenneth M. Case  
The Rockefeller University  
New York, New York 10021

Dr. Robert Cooper [2]  
Director, DARPA  
1400 Wilson Boulevard  
Arlington, VA 22209

Dr. Roger F. Dashen  
Institute for  
Advanced Study  
Princeton, NJ 08540

Dr. Russ E. Davis  
Scripps Institution  
of Oceanography  
(A-030), 301 NORPAX, UCSD  
La Jolla, CA 92093

Defense Technical Information [2]  
Center  
Cameron Station  
Alexandria, VA 22314

The Honorable Richard DeLauer  
Under Secretary of Defense (R&E)  
Office of the Secretary of  
Defense  
The Pentagon, Room 3E1006  
Washington, D.C. 20301

Director [4]  
National Security Agency  
Fort Meade, MD 20755  
ATTN: Mr. Richard Foss, A05

CAPT Craig E. Dorman  
Department of the Navy, OP-095T  
The Pentagon, Room 5D576  
Washington, D.C. 20350

CDR Timothy Dugan  
NFO10 Detachment, Sultland  
4301 Sultland Road  
Washington, D.C. 20390

Dr. Frank Fernandez  
ARETE Assoc.  
P.O. Box 350  
Encino, CA 91316

DISTRIBUTION LIST

(Continued)

Mr. Richard Gasparouic  
APL  
Johns Hopkins University  
Laurel, MD 20707

Dr. Larry Gershwin  
NIO for Strategic Programs  
P.O. Box 1925  
Washington, D.C. 20505

Dr. S. William Gouse, W300  
Vice President and General  
Manager  
The MITRE Corporation  
1820 Dolley Madison Blvd.  
McLean, VA 22102

Dr. Edward Harper [10]  
SSBN, Security Director  
OP-021T  
The Pentagon, Room 4D534  
Washington, D.C. 20350

Mr. R. Evan Hineman  
Deputy Director for Science  
& Technology  
P.O. Box 1925  
Washington, D.C. 20505

Dr. Richard Heglund  
Operations Research Inc.  
Room 428  
1400 Spring Street  
Silver Spring, MD 20910

Mr. Ben Hunter [2]  
CIA/DDS&T  
P.O. Box 1925  
Washington, D.C. 20505

The MITRE Corporation [25]  
1820 Dolley Madison Blvd.  
McLean, VA 22102  
ATTN: JASON Library, W002

Mr. Jack Kalish  
Deputy Program Manager  
The Pentagon  
Washington, D.C. 20301

Mr. John F. Kaufmann  
Dep. Dir. for Program Analysis  
Office of Energy Research, ER-31  
Room F326  
U.S. Department of Energy  
Washington, D.C. 20545

Dr. George A. Keyworth  
Director  
Office of Science & Tech. Policy  
Old Executive Office Building  
17th & Pennsylvania, N.W.  
Washington, D.C. 20500

Mr. Jerry King [3]  
RDA  
P.O. Box 9695  
Marina del Rey, CA 90291

MAJ GEN Donald L. Lamberson  
Assistant Deputy Chief of Staff  
(RD&A) HQ USAF/RD  
Washington, D.C. 20330

Dr. Donald M. Levine, W385 [3]  
The MITRE Corporation  
1820 Dolley Madison Blvd.  
McLean, VA 22102

Mr. V. Larry Lynn  
Deputy Director, DARPA  
1400 Wilson Boulevard  
Arlington, VA 22209

DISTRIBUTION LIST

(Continued)

Dr. Joseph Mangano [2]  
DARPA/DEO  
9th floor, Directed Energy Office  
1400 Wilson Boulevard  
Arlington, VA 22209

Mr. Walt McCandless  
4608 Willet Drive  
Annandale, VA 22003

Mr. John McMahon  
Dep. Dir. Cen. Intelligence  
P.O. Box 1925  
Washington, D.C. 20505

Director  
National Security Agency  
Fort Meade, MD 20755  
ATTN: William Mehuron, DDR

Dr. Marvin Moss  
Technical Director  
Office of Naval Research  
800 N. Quincy Street  
Arlington, VA 22217

Dr. Walter H. Munk  
9530 La Jolla Shores Drive  
La Jolla, CA 92037

Dr. Julian Nell [2]  
P.O. Box 1925  
Washington, D.C. 20505

Director  
National Security Agency  
Fort Meade, MD 20755  
ATTN: Mr. Edward P. Neuburg  
DDR-FANX 3

Prof. William A. Nierenberg  
Scripps Institution of  
Oceanography  
University of California, S.D.  
La Jolla, CA 92093

Dr. John Penhune  
Science Applications, Inc.  
MS-8  
1200 Prospect Street  
La Jolla, CA 92038

The MITRE Corporation  
Attn: Records Resources  
1820 Dolley Madison Boulevard  
McLean, VA 22102

Mr. Alan J. Roberts  
Vice President & General Manager  
Washington C<sup>3</sup> Operations  
The MITRE Corporation  
1820 Dolley Madison Boulevard  
Box 208  
McLean, VA 22102

Los Alamos Scientific Laboratory  
ATTN: C. Paul Robinson  
P.O. Box 1000  
Los Alamos, NM 87545

Mr. Richard Ross [2]  
P.O. Box 1925  
Washington, D.C. 20505

Mr. Richard Ruffine  
OUSPRE  
Offensive & Space Systems  
The Pentagon, Room 3E129  
Washington, D.C. 20301

Dr. Phil Selwyn  
Technical Director  
Office of Naval Technology  
800 N. Quincy Street  
Arlington, VA 22217

Dr. Eugene Sevin [2]  
Defense Nuclear Agency  
Washington, D.C. 20305

DISTRIBUTION LIST

(Concluded)

Mr. Robert Shaffer  
House Arms Services  
Room 2343  
Rayburn Office Building  
Washington, D.C. 20515

Mr. Omar Shemdin  
JPL  
Mail Stop 183501  
4800 Oak Grove Drive  
Pasadena, CA 91109

Mr. Robert Shuckman  
P.O. Box 8618  
Ann Arbor, MI 48107

Dr. Joel A. Snow [2]  
Senior Technical Advisor  
Office of Energy Research  
U.S. DOE, M.S. E084  
Washington, D.C. 20585

Mr. Alexander J. Tachmindji  
Senior Vice President & General  
Manager  
The MITRE Corporation  
P.O. Box 208  
Bedford, MA 01730

Dr. Vigdor Teplitz  
ACDA  
320 21st Street, N.W.  
Room 4484  
Washington, D.C. 20451

Mr. Anthony J. Tether  
DARPA/STO  
1400 Wilson Boulevard  
Arlington, VA 22209

Dr. Al Trivelpiece  
Director, Office of Energy  
Research, U.S. DOE  
M.S. 6E084  
Washington, D.C. 20585

Mr. Marshal Tulin  
Dept. of Mechanical Eng.  
University of California  
Santa Barbara, CA 93106

Dr. John F. Vesecky  
Center for Radar Astronomy  
233 Durand Building  
Stanford University  
Stanford, CA 94305

Mr. James P. Wade, Jr.  
Prin. Dep. Under Secretary of  
Defense for R&E  
The Pentagon, Room 3E1014  
Washington, D.C. 20301

Dr. Kenneth M. Watson  
2191 Caminito Circulo Norte  
La Jolla, CA 92037

Mr. Robert Winokur  
Director, Planning & Assess.  
Office of Naval Research  
800 N. Quincy Street  
Arlington, VA 22217

Mr. Leo Young  
OUSDRE (R&AT)  
The Pentagon, Room 3D1067  
Washington, D.C. 20301

Dr. Fredrik Zachariasen (452-48)  
California Institute  
of Technology  
1201 East California Street  
Pasadena, CA 91125



**END**

**FILMED**

**1-85**

**DTIC**